### OPTIMUM CONDITIONS OF A CARBON DIOXIDE TRANSCRITICAL POWER CYCLE FROM LOW TEMPERATURE HEAT SOURCE FOR POWER GENERATION.

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Centro tecnológico



Delft, The Netherlands Sept. 22 2011 José J. Segovia<sup>(1)</sup>, M. Carmen Martín<sup>(1)</sup>, Gregorio Antolin<sup>(2)</sup>, Cecilia Sanz<sup>(2)</sup>, Farid Chejne<sup>(3)</sup>.

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UVa







#### • INTRODUCTION.

- **DESCRIPTION OF THE CDTPC.**
- **MODELLING OF THE PROCESS.**
- **RESULTS AND DISCUSSION.**
- **CONCLUSIONS.**

### Introduction



➤ Worldwide energy demand is continuously increasing.



 $\times$  More than 50% of the fuel we use is waste.

But....

Conventional steam power cycles cannot give a better performance to recover low-grade waste heat.

➤ Organic Rankine Cycles show the known pinching problem.

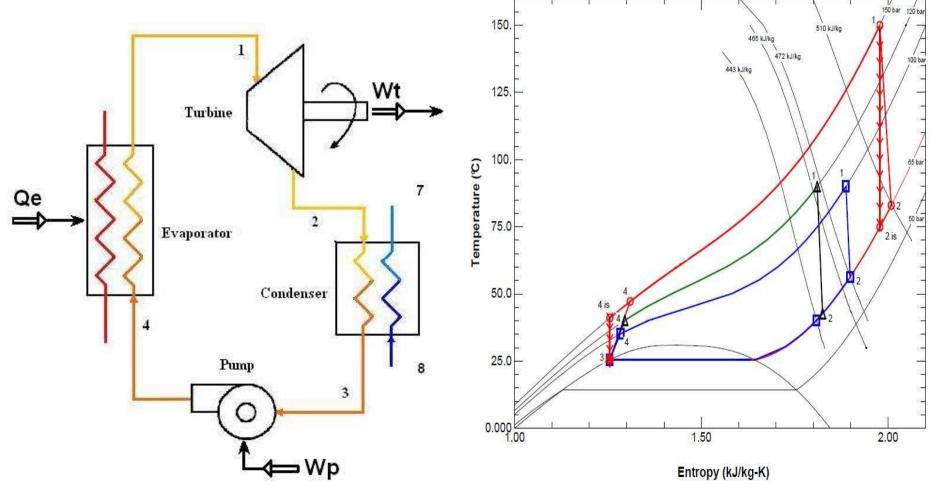
So.....

✓ Use of carbon dioxide in transcritical conditions in a Rankine cycles can solve both problems.

## **Description of the CDTPC**



Rankine cycle where the working fluid (CO<sub>2</sub>) goes through UVa
both subcritical and supercritical states, "a transcritical cycle".

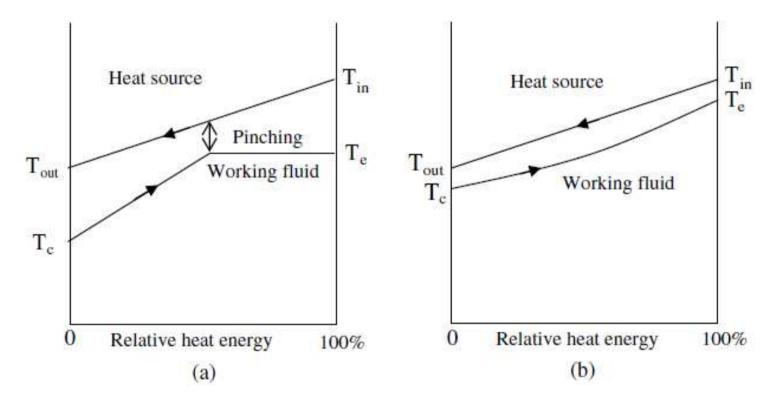




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 In the evaporator, it is obtained a better fit with the heat source when the heat is added to the working fluid in supercritical conditions.



Y. Chen et al. / Applied Thermal Engineering 26 (2006) 2142-2147

## **Modelling of the process**



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- Constant isentropic efficiencies of 75% are assumed for the pump as well as for the turbine.
- Steady state conditions.
- No pressure drop or heat loss in the evaporator, condenser or the pipes.
- An inlet temperature of the condensation water  $T_7=15$  °C.
- Working fluid condensation temperature  $T_3=25$  °C.
- Turbine inlet temperature  $T_1 = 150 \text{ °C}$ .
- Turbine inlet pressure P<sub>1</sub>, varying from 66 bar until the net work was **around** zero.

## Modelling of the process.



• The cycle's total energy efficiency is:

$$\eta = \frac{\dot{W_t} - \dot{W_p}}{\dot{Q_e}} \qquad \qquad \dot{W_t} = \dot{m} \times \eta_t \times (h_1 - h_2) \qquad \qquad \dot{W_p} = \dot{m} \times (h_3 - h_4) / \eta_p \\ \dot{Q_e} = \dot{m} \times (h_1 - h_4)$$

• The exergy efficiency is defined as:

$$\eta_E = 1 - \left(\frac{\sum_{i} \dot{I}_i}{\sum_{i} \dot{E}_{in,i}}\right)$$

 $I_i$  is the exergy loss (destruction) of each component i (evaporator, turbine, condenser and pump) that can be found from an exergy balance.

 $\dot{E}$  Exergy rate.



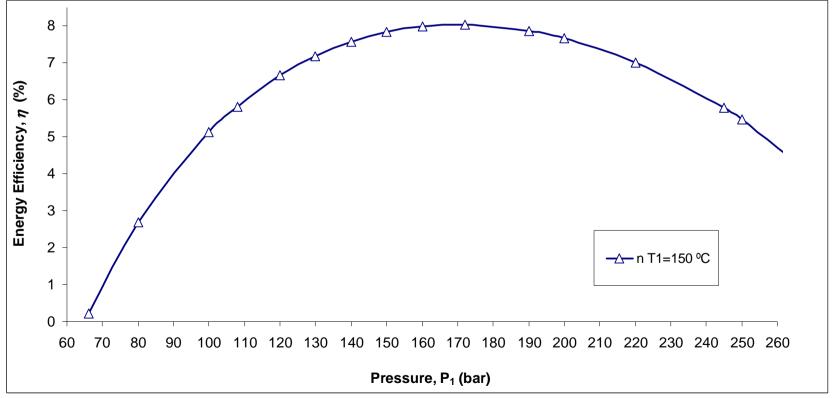
## **Results and discussion**



### ENERGY ANALYSIS



- Energy efficiency increases as pressure P<sub>1</sub> rises.
- A parabola-like behaviour.



Energy efficiency vs Pressure P<sub>1</sub> with an inlet temperature to the turbine at 150 °C.

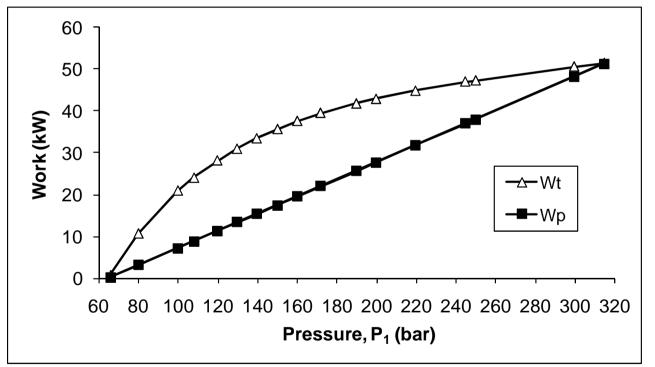




### ENERGY ANALYSIS



• Energy.



\*F. Vélez et al. / Energy 36 (2011) 5497-5507

#### Work produced and consumed by the turbine and the pump, respectively vs Pressure P<sub>1</sub> with an inlet temperature to the turbine at 150 °C.

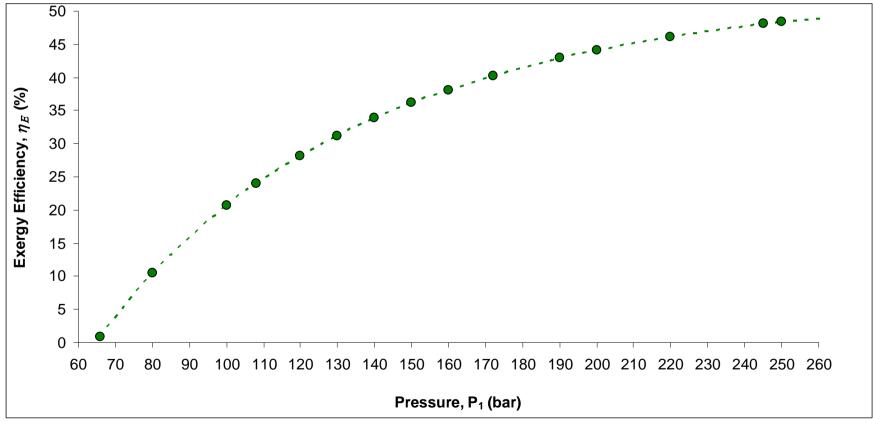
# **Results and discussion**



### EXERGY ANALYSIS



• Exergy.



Exergy efficiency vs Pressure P<sub>1</sub> with an inlet temperature to the turbine at 150 °C.

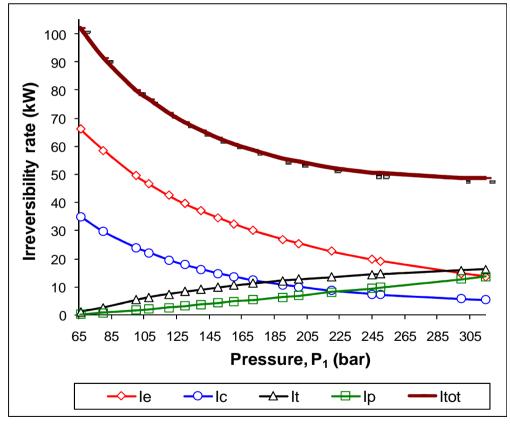


#### EXERGY ANALYSIS

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Irreversibilities of the process in each device.



<sup>\*</sup>F. Vélez et al. / Energy 36 (2011) 5497-5507

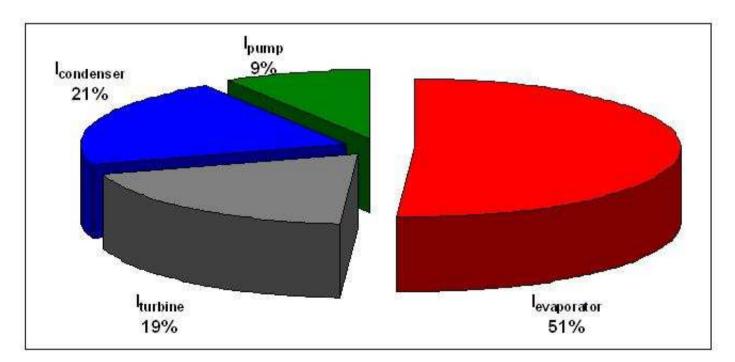
### Effect of the inlet pressure to the turbine over the irreversibilities of the process with an inlet temperature to the turbine at 150 °C.



#### EXERGY ANALYSIS



Irreversibilities of the process in each device at optimum conditions.



Irreversibilities of the process in optimum conditions with an inlet temperature to the turbine at 150 °C.







#### **Optimum conditions of design at** $T_1$ **=150°C.**

Parameter			
Pressure (bar)	η (%)	η <sub>Ε</sub> (%)	<i>wne</i> (kJ/kg)
172.0	8.0	40	17.5

✓ CDTPC is suitable for the production of useful energy utilising low enthalpy heat.

✓ It is possible to operate with a CDTPC in relatively low temperature ranges.

✓ Maximun point in the energy efficiency of the process is found.







#### Low temperature heat source for power generation:

### Exhaustive analysis of a carbon dioxide transcritical power cycle

#### \*F. Vélez et al. / Energy 36 (2011) 5497-5507

## THANK YOU FOR YOU ATTENTION.



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